



## O2k-SOP

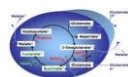
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# Instrumental background correction, accuracy of oxygen flux and SOP

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## 1. Introduction

For calibration of the polarographic oxygen sensor (POS) and measurement of instrumental background oxygen consumption, incubation medium without biological sample is added into the O2k-Chamber at experimental conditions. In a closed chamber under these conditions, ideally oxygen concentration remains constant. In practice, however, instrumental background effects are caused by backdiffusion into the

chamber at low oxygen pressure, oxygen diffusion out of the chamber at elevated oxygen levels, and oxygen consumption by the polarographic oxygen sensor (OroboPOS). Determination of instrumental background constitutes an important standard operating procedure (SOP) in high-resolution respirometry (HRR). Instrumental background oxygen flux is (i) minimized in the OROBOROS Oxygraph-2k by instrumental design and selection of appropriate materials. In addition, (ii) instrumental background is routinely tested, and (iii) background correction of oxygen flux is applied automatically by DatLab.

As an important component of quality assurance, instrumental background is monitored at regular intervals during an experimental project and documented, as a standard operational procedure to exclude instrumental artefacts. This SOP is implemented even in cases of high experimental oxygen fluxes when background correction is merely within 1%-5% of flux. Taken together, the concept of instrumental background oxygen flux and appropriate corrections are indispensable components of HRR. To obtain accurate parameters for instrumental background correction, background tests are performed in which several oxygen levels are set in the closed O2k-Camber related to the experimental oxygen regime, and background oxygen flux is measured as a function of oxygen concentration.

## 2. Preparations

### 2.1 Solutions

#### Dithionite solution (10 mM, in phosphate buffer):

Component	Final conc.	FW	Addition to 10 ml final
Na <sub>2</sub> S <sub>2</sub> O <sub>4</sub>	10 mM	174.1	0.017 g

#### Phosphate buffer (50 mM, pH 8):

	Final conc.	Component	FW	Addition to 1 liter final
Base	44 mM	Na <sub>2</sub> HPO <sub>4</sub> · 2 H <sub>2</sub> O	178.0	7.83 g
Acid	5.9 mM	NaH <sub>2</sub> PO <sub>4</sub> · H <sub>2</sub> O	138.0	0.81 g

Dithionite solution has to be prepared fresh and stored on ice immediately before use. Add 17 mg dry dithionite into a glass volumetric flask and add phosphate buffer to the final 10 ml volume. Keep the flask closed and minimize exposure to air.

## 2.2 Media

The dithionite background experiment has to be performed in MiR06 (or MiR05; [MiPNet14.13](#)). In many other media (including cell culture media and unbuffered water) side reactions lead to additional oxygen fluxes which interfere with the instrumental background oxygen flux. As an alternative, a strongly buffered alkaline phosphate buffer may be used (>100 mM); >pH 8). Results obtained in MiR06 can be used for other media (e.g. cell culture media).

## 2.3 Calibration of the oxygen sensors



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## 2.4 Experimental oxygen concentration

Graded levels of oxygen can be achieved in instrumental background tests with the aid of a gas phase included in the O2k-Camber, replacing air with nitrogen or argon (to decrease oxygen levels), or with oxygen (to increase oxygen levels). Mass transfer between gas and liquid phases proceeds until the targeted oxygen level is reached. This process is stopped when the gas phase is eliminated by closing the chamber (Gnaiger et al. 1995; Gnaiger 2008).

The main disadvantage of intermittently opening the O2k-Chamber for application of a gas phase during background experiments is the risk of inclusion of gas bubbles when closing the chamber. Elimination of gas bubbles is more difficult in [O2k-MultiSensor ISE](#) applications, when one or two additional electrodes are introduced through inlets in the stopper. Importantly, in these applications instrumental background correction is even more important, since inserted electrodes add new oxygen storage capacities and potential leaks.

An automatic O<sub>2</sub> background test has been introduced to overcome these problems with the [TIP2k](#).

Instrumental background tests should cover the entire experimental oxygen range. Most experiments are performed at oxygen levels below air saturation, but high oxygen levels are used with permeabilized fibres.

**H<sub>2</sub>O<sub>2</sub>:** With MiR06 (containing catalase) oxygen concentration is easily adjusted by injecting small amounts of a H<sub>2</sub>O<sub>2</sub> stock solution into the closed chamber ([MiPNet14.13](#)).

Oxygen levels are increased in steps of  $<200 \mu\text{M}$  (e.g. from air saturation up to  $350 \mu\text{M}$ ) to prevent formation of gas bubbles in the medium.

**O<sub>2</sub> (gas phase):** For oxygen concentrations above  $400 \mu\text{M}$ , the preferred approach is application of a gas phase with high oxygen pressure.



If a calibration at air saturation was just performed, there is already an 'open chamber', i.e. a chamber with a gas phase. Insert the stopper, completely closing the chamber. Siphon off any medium extruded through the stopper capillary. Then partially open the stopper (arrow 1), insert the stopper-spacer tool (2) and push down the stopper (3). The gas injection syringe with supplied needle (4; correct length) and spacer (5) is filled with oxygen gas. Inject a few ml of oxygen into the gas phase (6), thereby creating an elevated oxygen

pressure above the stirred aqueous medium. Oxygen in the gas and aqueous phases will start rapidly to equilibrate.

Observe the oxygen signal in DatLab carefully. When the desired oxygen concentration is nearly reached, close the chamber, thereby extruding the gas phase and stopping the equilibration process. After stabilisation of oxygen flux, the first state of background flux is recorded, by marking an appropriate section of the oxygen flux ([MiPNet19.01E](#)). Further steps of oxygen levels towards air saturation may be achieved by shortly opening the stopper (again using the stopper-spacer tool, 2), observing the drop of oxygen concentration and closing the chamber at the desired oxygen level. Preferentially, use the TIP2k method described below.

### 3. Instrumental background test

#### 3.1 TIP2k in feedback control mode

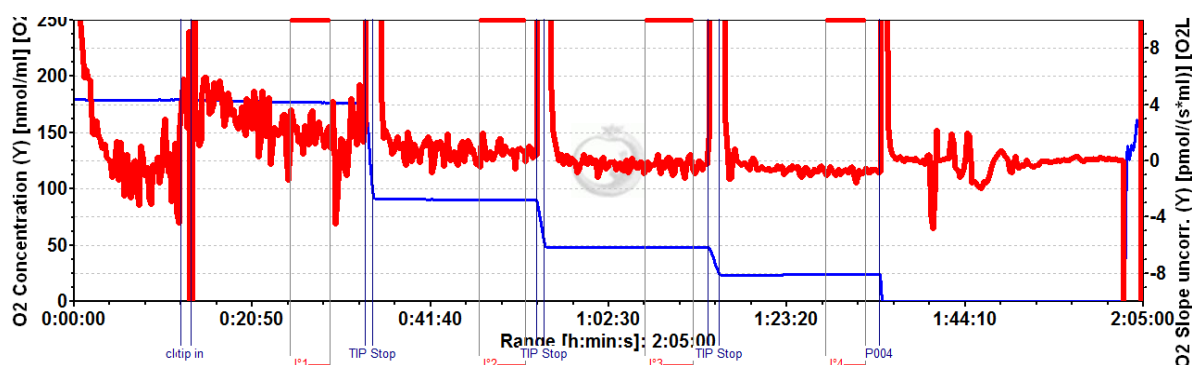
Fill the TIP2k syringes with the freshly prepared dithionite solution, rinsing the syringes at least once with the dithionite solution and taking care to minimize exposure of the dithionite solution to air. Use a large-volume glass syringe and long needle to fill both TIP2k syringes sequentially.

After air calibration close the chamber either directly (normoxia) or after elevating oxygen levels (hyperoxia). After closing the chamber, insert the TIP2k needles through the stopper.



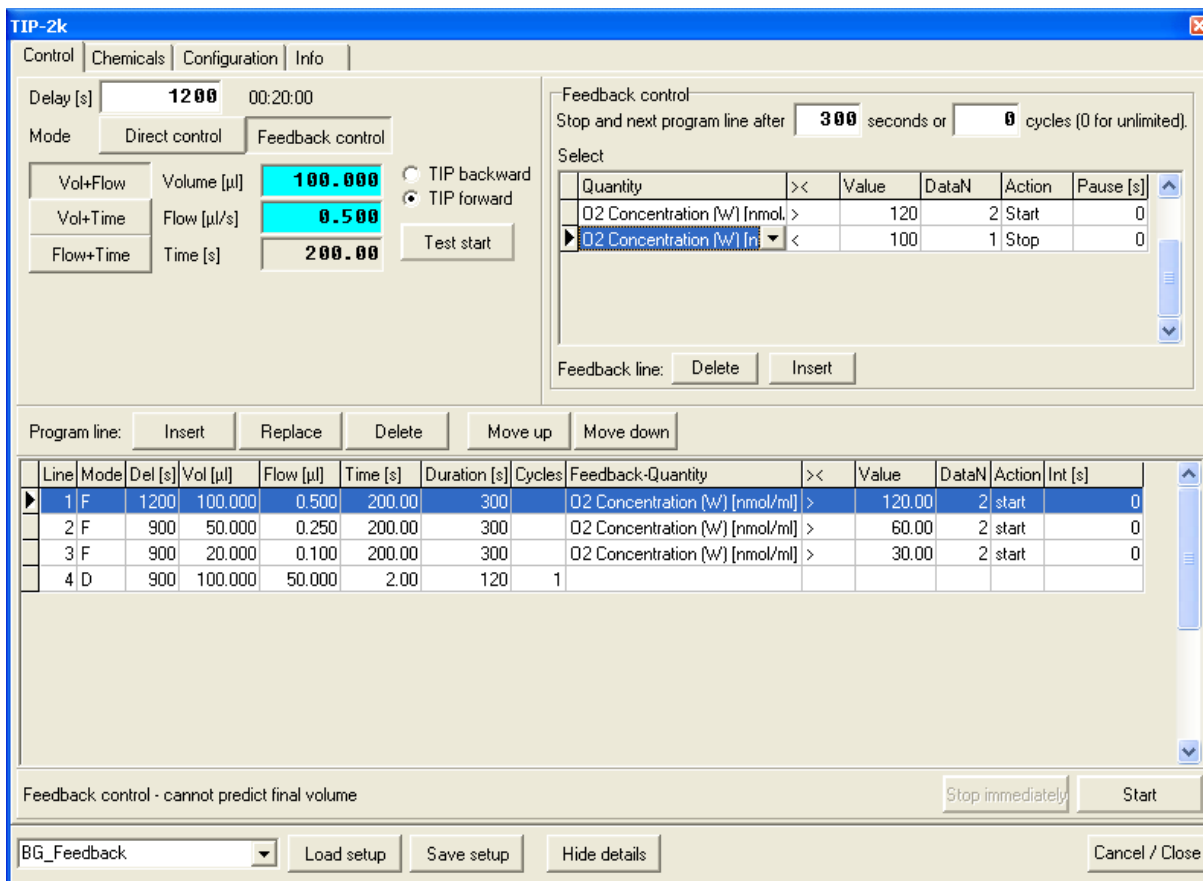
#### TIP2k-Manual:

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**TIP2k Setup "BG\_Feedback":** Instrumental background oxygen flux at air saturation (176  $\mu\text{M}$ ; 37  $^{\circ}\text{C}$ , 600 m altitude), 90  $\mu\text{M}$ , 45  $\mu\text{M}$ , 20  $\mu\text{M}$ . Each level was maintained for 20 minutes. The following parameters are used in the set up file:

Line	Mode	Start injection if oxygen level (left chamber) is >	Stop injection if oxygen level (left or right chamber) is <	Flow	Delay	Interval	Volume
		$\mu\text{M}$	$\mu\text{M}$	$\mu\text{l/s}$	s	s	$\mu\text{l}$
1	FB	120	100	0.5	1200	300	
2	FB	60	50	0.25	900	300	
3	FB	30	23	0.100	900	300	
4	D			40			100



In the DatLab main menu select "TIP", select "BG Feedback" ▼ from the dropdown menu and press "Load setup". Start the titration programme. During operation the TIP2k window may be closed.

The TIP2k programme starts, allowing for a delay of 1200 s (20 min), during which time oxygen flux can stabilize after closing the chamber, providing the first background level ( $J^{\circ 1}$ ). Then the first injection starts at 0.5  $\mu\text{l/s}$ . The TIP2k operates now in feedback mode while oxygen levels decline. The TIP2k stops when an O<sub>2</sub> concentration <100  $\mu\text{M}$  is reached, and possibly overshoots by 10  $\mu\text{M}$  to yield a level of about 90  $\mu\text{M}$  ( $J^{\circ 2}$ ). The 1200 s interval (20 min) is programmed as a feedback control time of 300 s plus a delay of 900 s before each further injection at 0.25  $\mu\text{l/s}$  to 50  $\mu\text{M}$  ( $J^{\circ 3}$ ) and 0.1  $\mu\text{l/s}$  to 23  $\mu\text{M}$  ( $J^{\circ 4}$ ) (reducing the overshoot to 5  $\mu\text{M}$  and 3  $\mu\text{M}$ ).

After recording the last background level ( $J^{\circ 4}$  at 20  $\mu\text{M}$ ) a final titration of excess dithionite is induced in the direct control mode for a zero oxygen calibration of the OroboPOS.

### 3.2 Manual injections

Use a Hamilton syringe for manually injecting the dithionite solution.

The effective concentration of dithionite decreases in the stock solution over time due to autoxidation when small amounts of oxygen leak into the solution. The potency of the solution can be tested by injecting a small volume (5 µl) into the closed oxygraph chamber and observing the change in oxygen concentration. The stoichiometric correction factor,  $SF$ , expresses the deviation of the effective dithionite concentration from the dithionite concentration added initially,

$$SF = \frac{\Delta n_{O_2}(\text{eff})}{\Delta n_{O_2}(\text{calc})} = \frac{\Delta c_{O_2} \cdot V_{\text{chamber}}}{v_{\text{inject}} \cdot c_{\text{Na}_2\text{S}_2\text{O}_4}} \quad (1)$$

$SF$	Stoichiometric correction factor for dithionite concentration
$\Delta n_{O_2}(\text{eff})$	Effective change of the amount of oxygen [µmol]
$\Delta n_{O_2}(\text{calc})$	Calculated change of the amount of oxygen [µmol]
$\Delta c_{O_2}$	Effective drop in oxygen concentration [µmol dm <sup>-3</sup> ; µmol.l <sup>-1</sup> ]
$V_{\text{chamber}}$	Chamber volume [cm <sup>3</sup> ; ml]
$v_{\text{inject}}$	Injected volume of dithionite solution [mm <sup>3</sup> ; µl]
$c_{\text{Na}_2\text{S}_2\text{O}_4}$	Dithionite concentration in the initial stock solution (approx. 9.8 mmol dm <sup>-3</sup> considering a complete consumption of oxygen originally dissolved in the aqueous solvent), irrespective of further oxygen uptake by the effectively anoxic solution.

$v_{\text{inject}}$  is the volume injected to achieve a specific drop in oxygen concentration:

$$v_{\text{inject}} = \frac{\Delta c_{O_2} \cdot V_{\text{chamber}}}{SF \cdot c_{\text{Na}_2\text{S}_2\text{O}_4}} \quad (2)$$

A typical value of  $SF$  is 0.7 in a freshly prepared stock solution. Since no accurate oxygen concentrations have to be achieved for determination of an instrumental background, a value of 0.7 can be used for most purposes. When using the TIP2k in Feedback Control Mode, calculation of  $SF$  is not necessary.

## 4. Analysis of instrumental background tests



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[MiPNet19.01E](#), [MiPNet08.09](#), [MiPNet10.04](#)

Gnaiger 2001 » ; 2008 » ; Gnaiger et al 1995 »

## 5. References

Gnaiger E (2008) Polarographic oxygen sensors, the oxygraph and high-resolution respirometry to assess mitochondrial function. In: Mitochondrial Dysfunction in Drug-Induced Toxicity (Dykens JA, Will Y, eds) John Wiley: 327-352. »

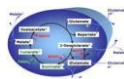
Gnaiger E (2001) Bioenergetics at low oxygen: dependence of respiration and phosphorylation on oxygen and adenosine diphosphate supply. *Respir Physiol* 128: 277-297. »

Gnaiger E, Steinlechner-Maran R, Méndez G, Eberl T, Margreiter R (1995) Control of mitochondrial and cellular respiration by oxygen. *J Bioenerg Biomembr* 27: 583-596. »



### O2k-Manual

- » [MiPNet19.01E](#) O<sub>2</sub> flux analysis: real-time.
- » [MiPNet12.10](#) Titration-Injection microPump. TIP2k user manual.



### O2k-Protocols

- » [MiPNet06.03](#) POS calibration, accuracy and quality control SOP.
- » [MiPNet08.09](#) HRR with leukemia cells: respiratory control and coupling.
- » [MiPNet10.04](#) HRR: Phosphorylation control in cell respiration.
- » [MiPNet14.13](#) Mitochondrial respiration medium – MiR06.



### Full version: go Bioblast

» [MiPNet14.06 InstrumentalBackground](#)

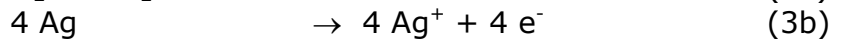




## Supplement A: Background parameters and accuracy of flux

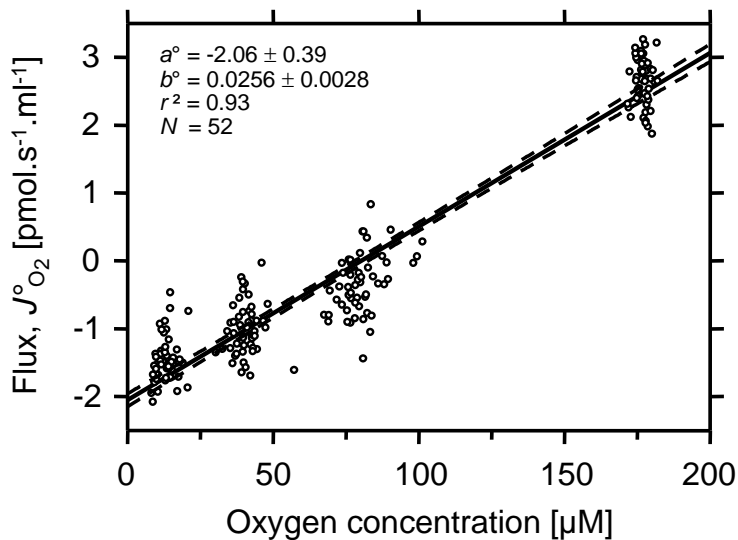
### Oxygen consumption by the polarographic oxygen sensor

The Clark-type polarographic oxygen sensor (POS) yields an electrical signal while consuming the oxygen which diffuses across the oxygen-permeable membrane to the cathode. The cathode and anode reactions are, respectively,



The electric flow (current,  $I_{\text{el}}$  [A]) is converted into a voltage (electric potential,  $V_{\text{el}}$  [V]) and amplified. In the Oxygraph-2k the gain,  $F_{\text{O}_2, \text{G}}$ , can be selected in DatLab within the Oxygraph setup menu, with values of 1, 2, 4, or  $8 \cdot 10^6$  V/A, where 1 V/ $\mu\text{A}$  is the basal gain at a gain setting of 1. The raw signal after amplification,  $R_{\text{O}_2}$  [V], is related to the original POS current,

$$I_{\text{el}} = R_{\text{O}_2} \cdot F_{\text{O}_2, \text{G}}^{-1} \quad (4)$$



**Figure 2.** Instrumental background oxygen flux,  $J^{\circ}_{\text{O}_2}$ , as a function of oxygen concentration,  $c_{\text{O}_2}$  [ $\mu\text{M}$ ], in the OROBOROS Oxygraph-2k (37 °C; NaCl solution with an oxygen solubility factor of 0.92 relative to pure water). Measurements in 52 chambers (2 ml volume) of 26 different instruments. In all tests, four oxygen ranges were selected consecutively in declining order. Each oxygen concentration was maintained for 20 min, at the end of

which, time intervals of 200 seconds (corresponding to 200 data points at the sampling interval of 1 s) were chosen for estimating average flux at each corresponding oxygen concentration. Averages and SD were calculated for the intercept,  $a^{\circ}$ , and the slope,  $b^{\circ}$ , by linear regression for each individual chamber. The full and stippled lines show the linear regression and 99 % confidence intervals calculated through all data points.

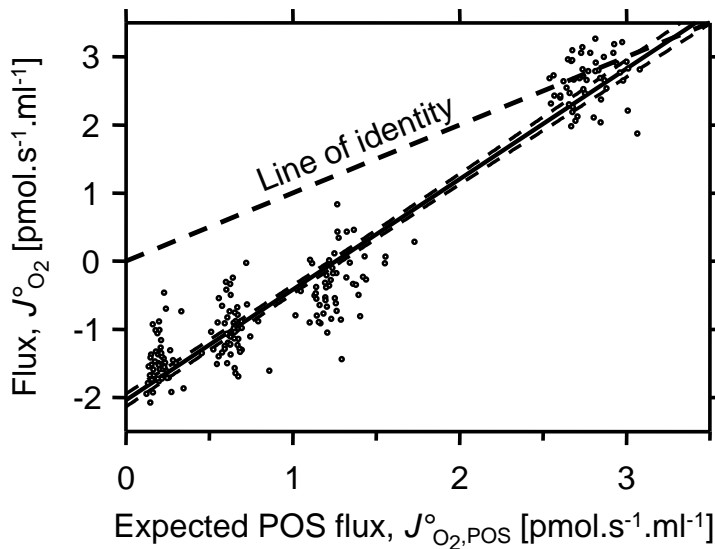
$R_{\text{O}_2}$  is about 9 V (at air saturation, 37 °C, and a gain of  $4 \cdot 10^6$  V/A), and is thus typically 2.2  $\mu\text{A}$  under these conditions. In the cathode reaction (Eq. 3a), electric flow,  $I_{\text{el}}$  [ $\text{A} = \text{C} \cdot \text{s}^{-1}$ ], is stoichiometrically related to molar oxygen flow,  $I_{\text{O}_2}$  [ $\text{mol O}_2 \cdot \text{s}^{-1}$ ], through the stoichiometric charge number of the reaction,  $\nu_{\text{e}^-/\text{O}_2} = 4$ , and the Faraday constant,  $F$ , i.e. the product of the elementary charge and the Avogadro constant ( $F = 96,485.53 \text{ C} \cdot \text{mol}^{-1}$ ; Mills et al., 1993). The oxygen/electric flow ratio is (Gnaiger, 1983),

$$\begin{aligned}
 Y_{O_2/e^-} &= (v_{e^-/O_2} \cdot F)^{-1} = (4 \cdot 96,485)^{-1} \text{ mol} \cdot \text{C}^{-1} & (5) \\
 &= 2.591068 \cdot 10^{-6} \text{ mol O}_2 \cdot \text{C}^{-1} \\
 &= 2.591 \text{ pmol O}_2 \cdot \text{s}^{-1} \cdot \mu\text{A}^{-1}.
 \end{aligned}$$

Oxygen consumption by the POS can be directly measured in the closed Oxygraph chamber at air saturation (Fig. 2), as volume-specific oxygen flux,  $J_{O_2}^\circ$  [ $\text{pmol} \cdot \text{s}^{-1} \cdot \text{cm}^{-3}$ ], and the corresponding theoretical oxygen flux in Eq.(3a) can be calculated,  $J_{O_2,POS}$  (Fig. 3),

$$J_{O_2,POS} = (R_{O_2} - R_{O_2,0}) \cdot Y_{O_2/e^-} \cdot F_{O_2,G}^{-1} \cdot V^{-1} \quad (6a)$$

where  $R_{O_2,0}$  is the raw signal at zero oxygen (zero current), and  $V$  is the chamber volume of the Oxygraph-2k ( $2 \text{ cm}^3$ ).



**Figure 3.** Instrumental background oxygen flux,  $J_{O_2}^\circ$ , as a function of the theoretical oxygen consumption by the polarographic oxygen sensor (POS), calculated from the electrical signal (current) as a function of oxygen concentration (from data in Figure 1). The line of identity (dashed) illustrates the full correspondence between experimental and theoretical oxygen consumption at air saturation (top right) and the increasing deviation at declining oxygen concentration owing to a linear increase of oxygen backdiffusion.

declining oxygen concentration owing to a linear increase of oxygen backdiffusion.

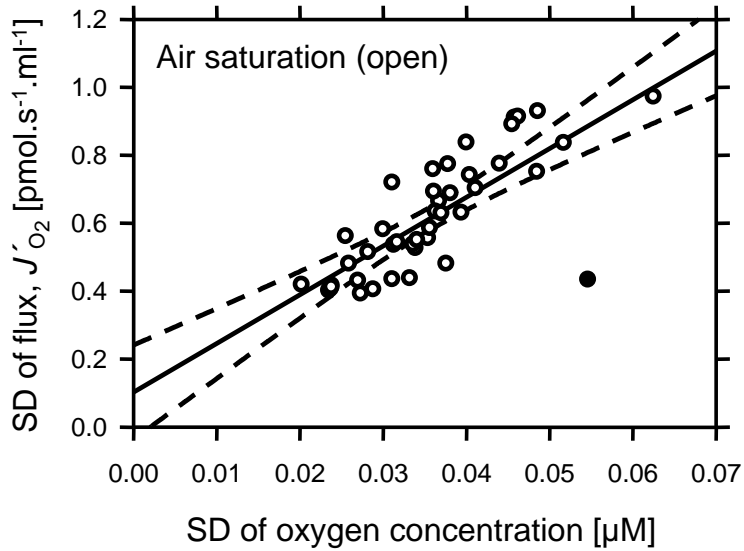
It is more convenient to relate the theoretical oxygen consumption of the POS to the measured oxygen concentration,  $c_{O_2}$  [ $\mu\text{M}$ ], using the oxygen calibration factor,  $F_{O_2,c}$  [ $\mu\text{M}/V$ ],

$$J_{O_2,POS} = (c_{O_2} \cdot F_{O_2,c}^{-1}) \cdot Y_{O_2/e^-} \cdot F_{O_2,G}^{-1} \cdot V^{-1} \quad (6b)$$

Combining constants from Eq. 5, at a gain setting of  $4 \text{ V}/\mu\text{A}$  and a volume of  $2 \text{ cm}^3$ , Eq. 6 is,

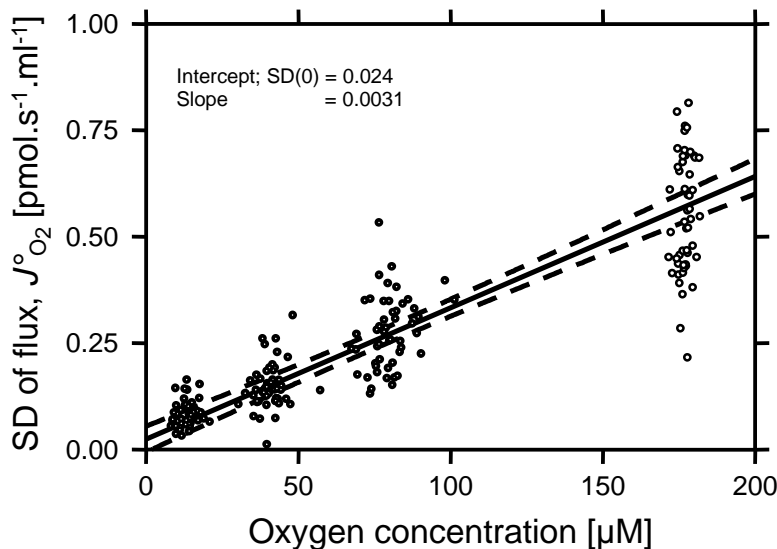
$$\begin{aligned}
 J_{O_2,POS} &= (R_{O_2} - R_{O_2,0}) \cdot 0.3239 \text{ pmol} \cdot \text{s}^{-1} \cdot \text{cm}^{-3} \cdot \text{V}^{-1} & (6c) \\
 &= c_{O_2} \cdot F_{O_2,c}^{-1} \cdot 0.3239 \text{ pmol} \cdot \text{s}^{-1} \cdot \text{cm}^{-3} \cdot \text{V}^{-1}
 \end{aligned}$$

**Figure 4.** Noise (SD of the mean) of the apparent oxygen flux,  $J'_{O_2}$ , as a function of noise (SD of the mean) of oxygen concentration,  $c_{O_2}$  ( $180 \pm 2 \mu\text{M}$ ; at  $95 \pm 1 \text{ kPa}$  barometric pressure), in the "open" chamber of the OROBOROS Oxygraph-2k ( $37 \text{ }^\circ\text{C}$ ; NaCl solution, at air saturation), over time intervals of 200 seconds (corresponding to 200 data points at the sampling interval of 1 s). Each data point ( $N=43$ ) represents an independent Oxygraph-2k chamber ( $2 \text{ ml}$  volume). The SD of oxygen concentration was calculated from the raw signal without smoothing. Flux was calculated from concentration smoothed with a moving average (30 data points), using an eight point polynomial for calculation of the slope. The outlier (full circle) corresponds to a data set with an individual spike.



The full and stippled lines show the linear regression and 99 % confidence intervals. On average, signal stability was indicated by apparent oxygen fluxes close to zero during air calibration, when oxygen concentration is maintained stable by exchange with the gas phase. Average  $J'_{O_2}$  amounted to  $0.04 \pm 0.14 \text{ pmol}\cdot\text{s}^{-1}\cdot\text{cm}^{-3}$  (range from  $-0.28$  to  $0.25 \text{ pmol}\cdot\text{s}^{-1}\cdot\text{cm}^{-3}$ ). To express signal noise independent of these low levels of signal

drift, linear regressions were calculated through these 200 second sections, and this drift was subtracted from the concentration before calculating the SD.



**Figure 5.** Noise (SD of the mean) of the instrumental background oxygen flux,  $J^{\circ}_{O_2}$ , as a function of oxygen concentration,  $C_{O_2}$  [ $\mu\text{M}$ ], in the OROBOROS Oxygraph-2k (37 °C; NaCl solution), over time intervals of 200 seconds (corresponding to 200 data points at the sampling interval of 1 s). Each data point ( $N=43$ ) represents an independent Oxygraph-2k chamber (2 ml volume). Flux was calculated from

concentration smoothed with a moving average (30 data points), using an eight point polynomial for calculation of the slope. The full and stippled lines show the linear regression and 99 % confidence intervals. To express noise of flux independent of small changes in flux over time, linear regressions were calculated through 200 second sections, and this trend was subtracted from flux before calculating the SD.

### Accuracy of instrumental background tests

Instrumental background interferes with accurate measurement of respiratory oxygen flux, if background effects remain undefined. The instrumental oxygen background parameters are a property of the O2k-Chamber. Any contamination of the medium causing oxidative processes (microbial respiration) is detected. Then background oxygen consumption is a property of a contaminated medium. Otherwise instrumental background does not depend on the specific medium. Therefore,

background parameters obtained in one medium can be used for another medium in the same chamber.

In a series of 52 experimental background determinations, 52 different O2k-chambers (2 ml volume, 37 °C) were tested (Oxygraph-2k, Series A). The following average conditions applied:

Oxygen concentration at air saturation,  $c_{O_2}^* = 179.9 \mu\text{M}$   
 Average oxygen concentration at  $J_{O_2,1}^0$ ,  $c_{O_2,1} = 177.2 \mu\text{M}$   
 Oxygen calibration signal at air saturation,  $R_{O_2,1} = 8.744 \text{ V (Gain 4)}$   
 Oxygen calibration signal at zero oxygen,  $R_{O_2,0} = 0.033 \text{ V (Gain 4)}$   
 Oxygen calibration factor,  $F_{O_2,c} = 20.69 \mu\text{M/V}$   
 $J_{O_2,POS} = 0.3239 \times 177.2/20.69 = 2.77 \text{ pmol}\cdot\text{s}^{-1}\cdot\text{cm}^{-3}$

At air saturation in the 2 cm<sup>3</sup> chamber, the theoretically expected oxygen consumption by the sensor is 2.77 pmol·s<sup>-1</sup>·cm<sup>-3</sup>, in direct agreement with the experimental result. At an average flux of 2.64 pmol·s<sup>-1</sup>·cm<sup>-3</sup> ( $\pm 0.35$  SD;  $N=52$ ; Fig. A2), the ratio between measured and theoretically expected oxygen consumption by the POS was 0.95 ( $\pm 0.12$  SD;  $N=52$ ). This provides possibly the first experimental evidence for the exact 4-electron stoichiometry in the reduction of oxygen at the cathode of the POS.

## Supplement B: TIP2k in direct control mode



### TIP2k-Manual

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Fill the TIP2k syringes with freshly prepared dithionite solution. After air calibration record the first point of the background experiment as described above.

**Programming the TIP2k:** Calculate the necessary injection volumes as described in Section 2.5, initially assuming  $SF = 0.7$  (stoichiometric correction factor for dithionite concentration).  $SF$  can be calculated after the first injection and – if necessary – the TIP2k be reprogrammed for subsequent injections. Alternatively,  $SF$  may be determined initially:

- Set the Volume,  $v_{\text{inject}}$ , to 5  $\mu\text{l}$ ;
- **Test start** before inserting the needles, to replace the dithionite solution in the needles;
- Wait for stabilisation of oxygen flux;
- Inject 5  $\mu\text{l}$  and calculate  $SF$  using Eq.(1).

**Example:** Oxygen level in the chamber is 160  $\mu\text{M}$ . The user wants to obtain four background levels (in addition to the one recorded near air saturation). With four evenly

spaced steps it is possible to reach a minimum of 20  $\mu\text{M}$  reducing the oxygen concentration by 35  $\mu\text{M}$  steps. The necessary injection volume,  $V_{\text{inject}}$ , to achieve the desired reduction of oxygen concentration can then be calculated from Eq.(2). In the present example:

$$SF = 0.7; \Delta c_{\text{O}_2} = 35 \mu\text{M}; V_{\text{chamber}} = 2 \text{ ml}; c_{\text{Na}_2\text{S}_2\text{O}_4} = 9.8 \text{ mM}$$
$$V_{\text{inject}} = 10 \mu\text{l}$$

Four injections of 10  $\mu\text{l}$  each should therefore bring the oxygen concentration near the desired last level of 20  $\mu\text{M}$ . Optionally, with a fifth injection, zero oxygen concentration could be reached. It is recommended to use a larger excess volume for zero calibration.

Always consider the expected experimental oxygen concentration range: For an experiment at high oxygen levels, calculate injection to decrease from the initial oxygen level (e.g. 350  $\mu\text{M}$ ) to the final oxygen concentration (e.g. air saturation). The minimum time required between injections to obtain stable fluxes is about 10 minutes. The time course of the instrumental background should match the decline of oxygen concentration in the real experiment. Longer intervals will typically be chosen (15 min in our example). The TIP2k can be set up in the following way:

Select **Direct control** and **Vol+Flow**

Delay [s]	0
Volume [ $\mu\text{l}$ ]	10
Flow [ $\mu\text{l}/\text{sec}$ ]	30
Interval [s]	900
Cycles	4

Start the experiment with **Start**.